



Original Research Paper

Combustion synthesis of $(\text{Mo}_{1-x}\text{Cr}_x)\text{Si}_2$ ($x = 0.00\text{--}0.30$) alloys in SHS modePeizhong Feng^{a,*}, Weisheng Liu^a, Akhtar Farid^b, Jie Wu^a, Jinan Niu^a, Xiaohong Wang^a, Yinghui Qiang^a^aSchool of Materials Science and Engineering, China University of Mining and Technology, Xuzhou 221116, PR China^bDepartment of Materials and Environmental Chemistry, Stockholm University, Stockholm 10691, Sweden

ARTICLE INFO

Article history:

Received 17 October 2010

Received in revised form 28 December 2010

Accepted 6 January 2011

Available online 18 January 2011

Keywords:

Molybdenum disilicide

Chromium alloying

Combustion synthesis

Self-propagating high-temperature synthesis

X-ray diffraction

ABSTRACT

Combustion synthesis was adopted to successfully synthesize molybdenum–silicon–chromium (Mo–Si–Cr) alloys by the mode of self-propagating high-temperature synthesis (SHS). The experimental study of combustion synthesis of Mo–Si–Cr alloys was conducted on elemental powder compacts. Powder compacts with nominal compositions including MoSi_2 , $(\text{Mo}_{0.95}\text{Cr}_{0.05})\text{Si}_2$, $(\text{Mo}_{0.90}\text{Cr}_{0.10})\text{Si}_2$, $(\text{Mo}_{0.85}\text{Cr}_{0.15})\text{Si}_2$, $(\text{Mo}_{0.80}\text{Cr}_{0.20})\text{Si}_2$, $(\text{Mo}_{0.75}\text{Cr}_{0.25})\text{Si}_2$ and $(\text{Mo}_{0.70}\text{Cr}_{0.30})\text{Si}_2$ were employed in combustion synthesis experiments. The combustion mode, combustion temperature, flame-front propagation velocity and product structure were investigated. The results showed that Mo–Si–Cr alloys were synthesized by an unsteady state combustion mode with a spiral-trajectory reaction front. The peak combustion temperature reduced with the addition of Cr to Mo–Si system. The flame-front propagation velocity decreased with an increase in Cr content of the powder compact. The X-ray diffraction (XRD) results showed that the crystal structure of the combustion product changed from C11_b -type structure $(\text{Mo}_{0.90}\text{Cr}_{0.10})\text{Si}_2$ to C40-type structure $(\text{Mo}_{0.85}\text{Cr}_{0.15})\text{Si}_2$ with increase in Cr content of Mo–Cr–Si alloys. The intensities of diffraction peaks of the C40-type phase gradually increased with increase in Cr content.

© 2011 The Society of Powder Technology Japan. Published by Elsevier B.V. and The Society of Powder Technology Japan. All rights reserved.

1. Introduction

MoSi_2 is a promising candidate material for high-temperature structural application owing to its high melting point (2303 K), excellent oxidation resistance at high temperatures (>1473 K), relatively low density (6.24 g/cm^3), lower coefficient of thermal expansion ($8.1 \times 10^{-6} \text{ K}^{-1}$), high thermal and electrical conductivities [1–3]. However, it has low fracture toughness at room temperature ($2\text{--}3 \text{ MPa}\cdot\text{m}^{1/2}$), low strength at high-temperature ($>$ brittle–ductile transition temperature) and poor oxidation resistance at about $500 \text{ }^\circ\text{C}$ (Pesting). Due to these disadvantages, its use in structural applications has been limited. Thus the key material issue is to improve its ductility at room temperature and strength at high temperature [2–4].

In metals, alloying is a major approach employed to increase room temperature fracture toughness. However, this has not been the case for structural ceramics because of the ionic-covalent bonding [1]. Alloying approaches to improve the toughness of structural silicides are, however, much more promising, due to the metallic-covalent bonding of these materials [1–3]. The effects of W, Ti, Re, Nb, Ta, Cr, Zr, V, and Al alloying additions on the microstructure and mechanical properties have been reported [1–8]. Yi et al. have prepared MoSi_2 -based alloys by the arc melting process from

high-purity metals. The EDS analysis showed that Fe, Co, and Ni had no solid solubility in as-cast MoSi_2 , while Cr, V, Ti, and Nb exhibit limited solid solubility, and solid solubility of Cr was determined to be $1.4 \pm 0.7 \text{ at.}\%$ [7]. However, Frankwicz et al. found that the solid solubility of Cr in MoSi_2 was about $3 \text{ at.}\%$ [7].

Harada et al. have prepared MoSi_2 , $(\text{Mo}_{0.985}\text{Cr}_{0.015})\text{Si}_2$, $(\text{Mo}_{0.97}\text{Cr}_{0.03})\text{Si}_2$ and $(\text{Mo}_{0.9}\text{Cr}_{0.1})\text{Si}_2$ button ingots, using a tri-arc furnace. The melting procedure was repeated six times [6]. Their results show that microhardness decreases slightly in the C11_b -type region; however, in two phase region of $\text{C11}_b + \text{C40}$ -type, the microhardness increases gradually with chromium content [6]. Single crystals of the nominal compositions of MoSi_2 and $(\text{Mo}_{0.97}\text{Cr}_{0.03})\text{Si}_2$ were grown using optical floating-zone furnace by Inui, Ishikawa, and Yamaguchi [5]. The Cr additions decreased the yield strength at low temperatures (below $800 \text{ }^\circ\text{C}$) and increased the yield strength at high temperatures (above $1300 \text{ }^\circ\text{C}$) [5].

Though MoSi_2 has excellent oxidation properties at high temperatures, it disintegrates catastrophically (termed as “Pesting”) during oxidation at low temperature ($400\text{--}600 \text{ }^\circ\text{C}$) [9–11]. From thermodynamic considerations, the third element X with a larger affinity to oxygen than Si (i.e. Al, Ti, Zr, and Y) is oxidized selectively at grain boundaries. In the case when the volume expansion during internal oxidation is small, the pesting phenomenon is suppressed [9–12]. The specimens of MoSi_2 , $(\text{Mo}_{0.90}\text{Cr}_{0.10})\text{Si}_2$ and $(\text{Mo}_{0.85}\text{Cr}_{0.15})\text{Si}_2$ were prepared by sintering in hydrogen at $1615 \text{ }^\circ\text{C}$. Oxidation tests were performed for 456 h (three weeks)

* Corresponding author. Tel./fax: +86 516 83591870.

E-mail address: fengroad@163.com (P. Feng).