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# Premature failure analysis of forged cold back-up roll in a continuous tandem mill

Hamid Reza Bakhsheshi Rad<sup>a,\*</sup>, Ahmad Monshi<sup>a</sup>, Mohd Hasbullah Idris<sup>b</sup>, Mohammed Rafiq Abdul Kadir<sup>b</sup>, Hassan Jafari<sup>b,c</sup>

<sup>a</sup> Materials Engineering Dept., Islamic Azad University, Najafabad branch, Isfahan, Iran

<sup>b</sup> Materials Engineering Dept., Faculty of Mechanical Engineering, Universiti Teknologi Malaysia, Skudai 81310, Johor, Malaysia

<sup>c</sup> Materials Engineering Dept., Faculty of Mechanical Engineering, Shahid Rajaee Teacher Training University, Tehran 16785-136, Iran

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#### ABSTRACT

In this paper, premature failure of a forged back-up roll from a continuous tandem mill was investigated. Microstructural evolutions of the spalled specimen and surface of the roll were characterized by optical microscopy, X-ray diffraction, scanning electron microscopy and ferritscopy, while hardness value of the specimen was measured by Vickers hardness testing. The results revealed that the presence of pore and MnS inclusion with spherical and oval morphologies were the main contributing factors responsible for the poor life of the back-up roll. In addition, metal pick up and subsequently strip welding on the surface of the work roll were found as the major causes of failure in work roll which led to spalling occurrence in the back-up roll. Furthermore, relatively high percentage of retained austenite, say 9%, in outer surface of the back-up roll contributed spalling due to conversion of this meta-stable phase to martensite and creation of volume expansion on the outer surface through work hardening during mill campaign.

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## 1. Introduction

In rolling mill operation a four roll high stand tandem mills including two work rolls and two back-up rolls are used to reduce force and power of work roll as well as increase the accuracy and thickness uniformity of thin sheets. Back-up rolls are the main trait of hot and cold roll mills which decrease unintended bending and support the work rolls, enabling them to endure higher loads without failing [1]. Work roll reduces the thickness of strip by plastic deformation which creates by high compressive stress via the rolls. Generally, steel material used for back-up roll is refined in electric arc furnace followed by vacuum degassing. The produced ingot is then forged and subsequently differential heat treatment is performed in order for the material to withstand the campaign in milling. Repeated loading under bending and compressive stresses, severe friction and wear under corrosive environments at high temperatures are some conditions that back-up rolls should endure during mill campaign [2,3].

The main reason for premature failure of the forged back-up roll can be the combined effects of mechanical and metallurgical factors. Mechanical factors include rolling parameter misalignment, uneven roll surface, lubrication, bearing, rolling speed seizure, insufficient stock removal during grinding and the experience of operators [4,5]. Metallurgical factors comprise the presence of non-metallic inclusions, localized overloading, casting defects, temperature gradients due to insufficient cooling and phase transformations [5,6]. It was observed [6] that spalling, cracking, metal pick up and subsequently strip welding are three critical factors responsible for the poor service life of back-up and work rolls during milling operation.

Spalling can be classified into two types. The first type is surface initiated spalling, which is identified by fatigue path accompanied arrest marks, originate from thermally crack or mechanically indentation, and subsequently fatigue path propagates circumferentially opposite to the direction of roll rotation. The second one, sub-surface initiated spalling, which is recognized by the presence of a concentric fatigue pattern (fish eye) on the fracture surface with arrest marks in the form of oval pattern, originates from a material defect and propagates in different directions away from the initiation site usually within a single plane of propagation [3]. In the present study the premature failure of a forged backup cold roll used for continuous tandem cold strip rolls was investigated. The main factors affecting the premature failure of the forged back-up roll were determined and analyzed [3,7].

## 2. Experimental procedure

A spalled sample from a forged back-up roll used in a 5 stand 4 Hi tandem mill was investigated. The chemical composition and detailed specifications of the forged back-up and work cold rolls are given in Tables 1 and 2, respectively. The sample was washed thoroughly with running distilled water, rinsed and ultrasonically degreased with acetone and dried. Afterwards, it underwent



<sup>\*</sup> Corresponding author. Tel.: +60 147382258; fax: +60 75534610 *E-mail address:* Rezabakhsheshi@gmail.com (H.R.B. Rad).

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